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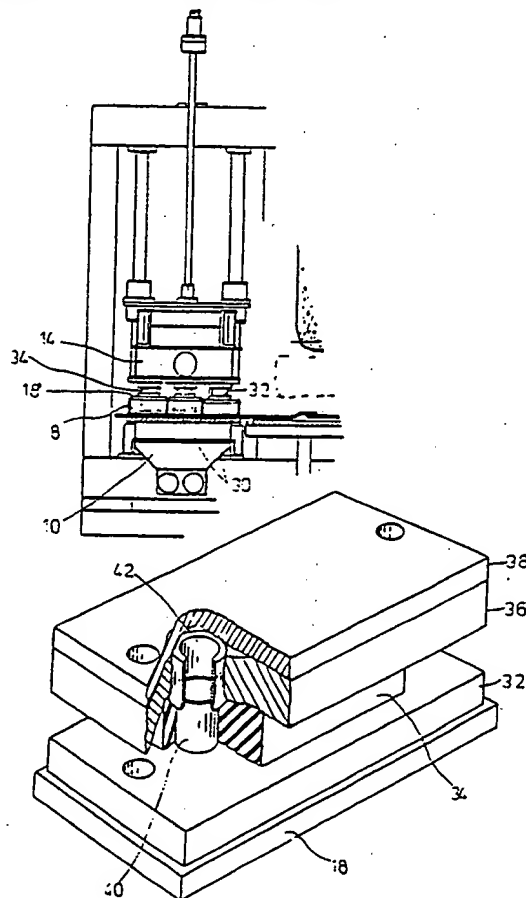
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tent), SU, TD (OAPI patent), TG (OAPI patent), US.**Published***With international search report.**In English translation (filed in Danish).*(54) Title: METHOD AND DEVICE FOR DIE-CASTING OF CONCRETE PRODUCTS SUCH AS BLOCK STONES  
IN A CELLULAR Mould

## (57) Abstract

At the casting of block stones in a cellular mould (8) it is customary to fill up the cells (30) completely with casting concrete, whereafter a holder-on (14) with load plates (18) corresponding to the cross section of the individual cells is pressed down against the mould for compression of the concrete in the individual cells. Hereby a uniform thickness of the cast members is achieved within a fairly extensive tolerance range, but not a uniform strength of these, as their contents of air varies. To achieve a prescribed strength of also the least compressed members, generally an overdose of cement for the concrete has to be used. By the invention a holder-on (14) is used, the load plates (18) of which are individually moveable in the pressure direction in such a manner that they will compress the concrete in the cells in a fairly similar way, i.e. for achievement of a fairly uniform strength of the members, which conditions a minimized admixture of cement. The compressed stone members will show mutually different heights, but it has been found that these height variations can be kept within the prescribed tolerance range of the stone height. The individual movability of the load plates (18) is obtained by these plates either being mounted on individual pressure cylinders or supported by springs such as rubber blocks (34).



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Method and device for die-casting of concrete goods  
such as block stones in a cellular mould.

The present invention relates to a method for die-casting  
of concrete goods such as block stones, which are cast in  
a cellular casting mould by this being completely filled with  
concrete, whereafter a superjacent holder-on or dolly  
5 provided with mutually flush load plates having a shape  
corresponding to the respective subjacent cell shapes is  
pressed down against the concrete surface for compression  
of the casting material in the individual cells, preferably  
during vibration of the casting material from the underside  
10 of the mould. After the required compression, the dolly is  
lifted from the mould, and the moulded stone bodies are  
demoulded.

For the supply of concrete to the mould cells, a so-called  
filler cart is normally used, which with its bottom open is  
15 deplaced from a position in which it is placed on a fixed  
bottom plate underneath the outlet for casting concrete  
from a silo, whereby it will bring a charge of concrete over  
the mould and during its return movement scrape off the  
excess amount of concrete for which there has been no room  
20 in the cells. Thus, the mould is left with a smooth concrete  
surface in level with the upper edges of the partitions  
between the cells.

Thereafter, the downwards pressing of the dolly is effected,  
e.g. by hydraulic power, the dolly being moved parallelly  
25 for obtaining that all the stones are compressed to the same  
height. Because of variations of the processing conditions  
and of the character of the casting concrete, the height of  
the stones will not always be the same, but as a height  
variation of  $\pm 2$  mm is normally accepted, the result will  
30 almost always be usable anyway.

The stones must meet the requirement that their strength

must be as good as possible, and that there must be only a small variation of the strength of the different stones of the production. As a certain stone strength variation inevitably occurs, the problem occurs in practice that for ensuring a desired minimum strength, it is necessary to use so much cement in the casting concrete that the weakest stones have the concerned minimum strength, whereby the other stones within the scope of variation will have an unnecessarily high cement content, i.e. generally the production requires an in reality unnecessarily high consumption of cement, which is a considerable disadvantage, economically as well as resource-wise.

The invention, which aims at fighting this disadvantage, is based on the consideration that the strength of the stone bodies is proportional to their density, and that thus, the strength variation will primarily be a question of density variations in the achieved result of the compression. By effecting that the density variations are equalized, the cement may thus be dosed in a better optimized manner for obtaining a cement economy in the running production, which justifies even a rather costly modification of the mould equipment.

The said stone strength variation is primarily caused by the fact that by the used simple method of casting concrete supply, an entirely uniform or compact filling of the cells is not obtained, as, locally, there may be more or less air in the concrete, and as this air only escapes by the compression and the vibration of the concrete, it is not possible in advance to effect any individual adjustment for obtaining a uniform result.

The invention is furthermore based on the observation that the normally occurring variation in the weight quantity of concrete of a uniform and good quality filled into the cells amounts to appx. 4%, which by an individually

impressed compression pressure of a normal magnitude gives a resulting height difference of appx. 3mm for typical block stones. When the products are compressed to the same height, the best filled cells will correspondingly give products having the highest density and thus the best strength. What is noticable here, however, is that the said height difference between products which have been individually compressed and thereby compressed to more or less the same density and strength is smaller than the pre-accepted height difference tolerance. This means that by controlling the production fairly closely with respect to concrete quality and processing parameters, it is necessary to use only a small part of the thickness tolerance for those variations which are caused by these conditions, while the rest of the tolerance interval may be used for obtaining a uniform density and strength by effecting an individual compression of the concrete in the different cells, whereby it is possible to continue using the said, very simple concrete supply method.

Thus, by the invention care is taken that the load plates of the dolly are pressed against the concrete in the individual cells with primarily the same force, but in a mutually independent manner with regards to movement. This may be obtained by each load plate being placed individually on an operation cylinder, these cylinders being carried on a common dolly base and supplied with pressure from the same pressure source, but as in practice only relatively small thickness variations for the stone members are concerned, it is fully sufficient to use load plates which are connected to the common dolly base through resiliently compressible means. These may easily be shaped such that for the resulting pressure force it will be of no special importance whether the load plate penetrates a few millimeters more or less down into the mould cells.

In the following, the invention, which also comprises the

concerned moulding equipment, is described in more detail with reference to the drawing, in which

Fig. 1 is a side view of a conventional production system for concrete block stones, shown during filling of the casting mould,

Fig. 2 is a section of the same view shown with the filler cart removed from the mould and with a dolly modified according to the invention, and

Fig. 3 is a detailed view of a part of the dolly by another embodiment of the invention.

The system shown in Fig. 1 comprises as main components a conveyor 2 for mould base plate members 4 fetched from a storage 6, a cellular mould 8 conveyed in a manner not shown to a base plate member 4 in a moulding station upon a vibro table 10, and underneath a carrier construction 12 for a dolly 14 having downwardly projecting pistons 16 for insertion down into the individual moulding cells in the mould 8. For this purpose the pistons 16 are provided with lower load plates 18 which may be exchangeable, and the shape of which corresponds to the cross sectional shape of the moulding cells, which may have a simply rectangular shape or various more complex shapes.

As further main components are provided a silo 20 for ready-mixed casting concrete, and a downwardly open filler cart 22, which by means of a moving mechanism 24 is movable back and forth between a position underneath an openable bottom outlet 26 of the silo 20, where the filler cart is supported on a fixed bottom plate member 28, and the shown position on top of the casting mould 8, in which position the casting concrete in the filler cart may sink down into the cells in the casting mould 8. When the filler cart 22 is thereafter moved back to the position underneath the silo 20 it will scrape the top surface of the mould 8

clean from excess casting concrete, such that the cells therein, designated 30, will be entirely filled with concrete.

Thereafter the vibro table 10 is started, and the dolly 14 is lowered until the load plates 18 engage the top surface of the concrete in each of the moulding cells 30. The dolly 14 is forced further downwards by hydraulic action, such that the load plates 18 have a compressing effect on the simultaneously vibrated concrete material in the mould cells 30. Optionally, also the dolly 14 may contain a vibrator.

By the invention the rigid pistons 16, 18 on the dolly 14 are replaced by either separately activatable pistons or - preferably - resiliently yielding pistons, which is illustrated in Fig. 2, where the dolly 14 is shown in its lowered position after withdrawal of the filler cart 22. The load plates 18 will now compress the casting material with practically the same force in all the moulding cells 30, and the final result will be that the ready-pressed stone members may have mutually different heights, but more or less the same density and strength, while the height variation of the stones will be within the thickness interval which is already generally acceptable.

In Fig. 3 is shown a preferred embodiment of the pistons depending from the dolly 14, the pistons being terminated lowermost by the said load plate 18, which may be of a rectangular or any other relevant shape. The load plate 18 is screwed on to a thrust pad 32 which is fastened to the underside of a rubber block 34, which at its top side is fixed to a plate block 36 fastened to the underside of a lower carrier plate 38 of the dolly 14. Near a peripheral area of the resilient block 34 an upwardly projecting guide pin 40 is placed on the thrust pad 32, the guide pin extending upwards through a hole in the rubber body 34 and

being received in an optionally pipe lined cavity 42 provided in the plate block 36, whereby the thrust pad 32 with the load plate 18 is kept from being rotatable relative the carrier plate 38, while it may move up and  
5 down unobstructed relative this plate by resilient compression of the body 34.

For ensuring a correct function of the equipment, position sensors may be used for sensing the position of both the dolly 14 in general and the thrust pads 32 individually.  
10 It should be ensured that all the thrust pads are activated by compression of the rubber blocks 34 to a position corresponding to a predetermined dolly pressure, and that none of the thrust pads are "pressed home" after a further travel of slightly less than the general thickness  
15 tolerance for the produced goods, e.g. 3-3½ mm by a tolerance of 4 mm.



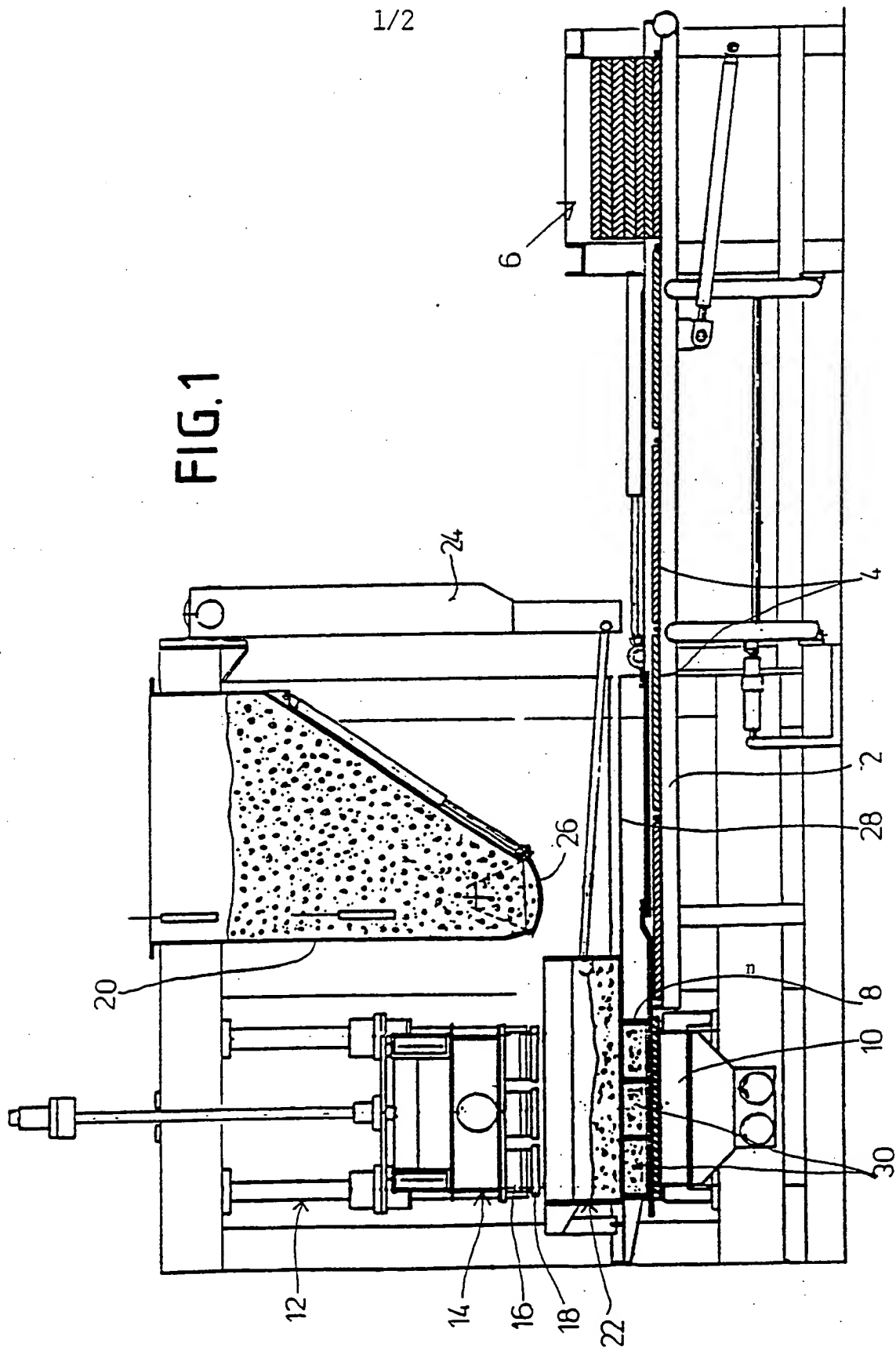
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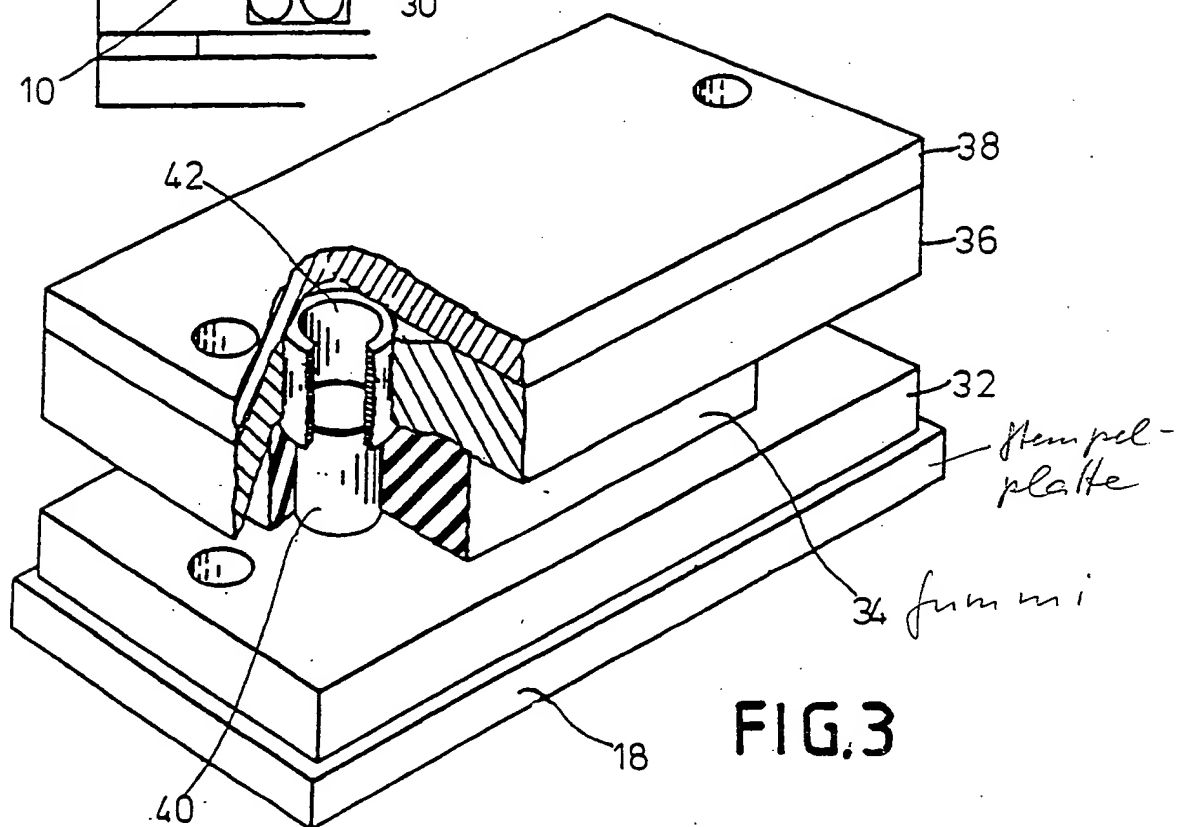
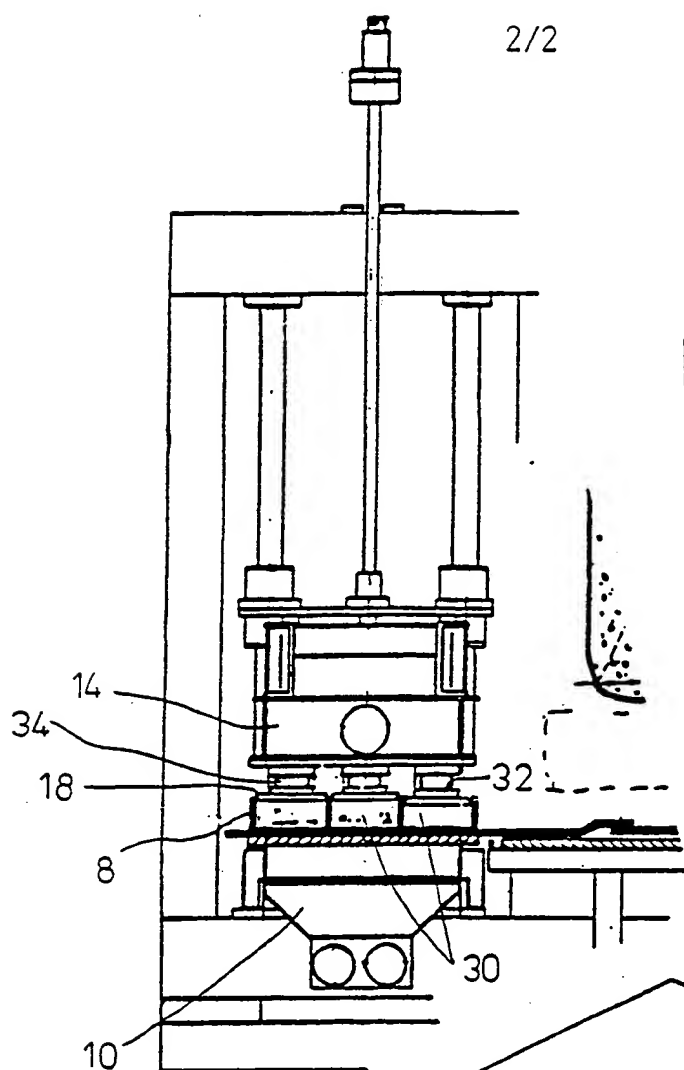
1. A method for die-casting of concrete goods such as block stones which are cast in a cellular casting mould by the cells of this being filled completely with concrete, whereafter a superjacent holder-on or dolly provided with mutually flush load plates having a shape corresponding to the respective subjacent cell shapes is pressed down against the concrete surface for compression of the casting material in the individual cells, characterized in that a dolly is used which has load plates which are individually movable in the pressure direction by the effect of individual pressure exerting means for affecting the load plates with more or less the same pressure, or by means of springs, respectively, which springs allow the load plates to yield individually by the collective pressing against the concrete surfaces in the cells, and that this dolly is pressed down to a position in which the occurring height differences between the load plates lies within the acceptable thickness variation scope for the produced bodies.
2. A system for implementing the method according to claim 1, comprising a cellular casting mould and means for supplying casting concrete thereto for complete filling of the cells with concrete, and a superjacent dolly provided with mutually flush load plates having a shape corresponding to the cross sectional shape of the respective subjacent mould cells, which dolly is downwardly pressable against the casting mould for compression of the concrete in the individual cells, characterized in that the load plates are placed individually movably on the dolly for impression against the concrete surfaces with a primarily uniform force per surface unit, the load plates either being separately downwardly pressable from the dolly, e.g. by a uniform hydraulic effect, or being positioned so as to be resiliently impressible against the dolly.

3. A system according to claim 2, characterized in that the load plates are placed on the dolly with an intermediate layer of a resilient block material.

FIG. 1

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Form PCT/ISA/210 (second sheet) (January 1985)

## FURTHER INFORMATION CONTINUED FROM THE SECOND SHEET

II

Fields searched (cont)

US C1 425: 167, 344, 352, 355, 357, 358, 406,  
417, 421, 424;

264: 297, 308, 319, 333

V. ☐ OBSERVATIONS WHERE CERTAIN CLAIMS WERE FOUND UNSEARCHABLE <sup>1</sup>

This international search report has not been established in respect of certain claims under Article 17(2) (a) for the following reasons:

1. ☐ Claim numbers ..... because they relate to subject matter not required to be searched by this Authority, namely:

2. ☐ Claim numbers ..... because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:

3. ☐ Claim numbers ..... because they are dependent claims and are not drafted in accordance with the second and third sentences of PCT Rule 6.4(a).

VI. ☐ OBSERVATIONS WHERE UNITY OF INVENTION IS LACKING <sup>2</sup>

This international Searching Authority found multiple inventions in this international application as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims of the international application.

2. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims of the international application for which fees were paid, specifically claims:

3. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claim numbers:

4. ☐ As all searchable claims could be searched without effort justifying an additional fee, the international Searching Authority did not invite payment of any additional fee.

## Remark on Protest

☐ The additional search fees were accompanied by applicant's protest.

☐ No protest accompanied the payment of additional search fees.